Heat transfer processes using viscoelastic fluids in laminar and turbulent regimes PhD Student Laura Moreno

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Introduction: Viscoelasticity

What is viscoelasticity?

- Fluids depending on their behaviour under the action of shear stress, can be classified as Newtonian and non-Newtonian.
- Viscoelastic fluids are a specific type of non-Newtonian fluids that exhibits a combination of elastic and viscous effects.
	- Visco: friction, irreversibility, loss of memory.
	- Elastic: recoil, internal energy storage.
- They have "memory": the state-of-stress depends on the flow history.

Introduction: Viscoelasticity

Other industry applications

• Most viscoelastic fluids are made of, or contain polymers (polymer solutions and polymer melts).

Introduction: Modelling of polymeric fluids

Like all fluids, viscoelastic fluids are governed by:

• Momentum equation:

$$
\rho \frac{\partial \mathbf{u}}{\partial t} + \rho \mathbf{u} \cdot \nabla \mathbf{u} - \nabla \cdot \mathbf{T} + \nabla p = \mathbf{f}
$$

• Continuity equation: $\nabla \cdot \mathbf{u} = 0$

For Newtonian viscous fluids: $\mathbf{T} = \eta(\nabla \mathbf{u} + \nabla^t \mathbf{u})$

For Polymeric fluids: $\mathbf{T} = \eta_{\mathbf{s}}(\nabla \mathbf{u} + \nabla^t \mathbf{u}) + \boldsymbol{\sigma}$

Introduction: Constitutive models.

$$
\rho \frac{\partial \boldsymbol{u}}{\partial t} + \rho \boldsymbol{u} \cdot \nabla \boldsymbol{u} - \nabla \cdot \mathbf{T} + \nabla \rho = \boldsymbol{f} \text{ in } \Omega, t \in]0, t_f[,
$$

$$
\nabla \cdot \boldsymbol{u} = 0 \text{ in } \Omega, t \in]0, t_f[,
$$

$$
\frac{\lambda}{2\eta_0} \frac{\partial \sigma}{\partial t} - (1 - \beta) \nabla^s \boldsymbol{u} + \frac{\lambda}{2\eta_0} (\boldsymbol{u} \cdot \nabla \sigma - g(\boldsymbol{u}, \sigma))
$$

$$
\frac{1}{2\eta_0} (1 + h(\sigma)) \cdot \sigma = 0 \text{ in } \Omega, t \in]0, t_f[,
$$

where $g(\bm u,\bm \sigma) = \bm \sigma \cdot \nabla \bm u - (\nabla \bm u^{\sf T}) \cdot \bm \sigma$ and $\bm{\mathsf{T}} = 2\beta\eta_0\nabla^{\sf s}\bm u + \bm \sigma.$

Oldroyd-B $h(\sigma) = 0$ Giesekus $h(\boldsymbol{\sigma}) = \frac{\epsilon \lambda}{\eta_{\boldsymbol{\rho}}} \boldsymbol{\sigma}$ Phan-Thien-Tanner $h(\boldsymbol{\sigma}) = \frac{\epsilon \dot{\lambda}}{\eta_{\boldsymbol{\rho}}} \mathsf{tr}(\boldsymbol{\sigma})$

Introduction: The Weissemberg number

$$
\frac{\lambda}{2\eta_0}\frac{\partial \boldsymbol{\sigma}}{\partial t}-(1-\beta)\nabla^s\boldsymbol{u}+\frac{\lambda}{2\eta_0}\left(\boldsymbol{u}\cdot\nabla \boldsymbol{\sigma}-g(\boldsymbol{u},\boldsymbol{\sigma})\right)+\frac{1}{2\eta_0}(1+h(\boldsymbol{\sigma}))\cdot \boldsymbol{\sigma}=\boldsymbol{0}
$$

$$
\mathsf{We} = \lambda \frac{U}{L}
$$

- When We is small we have Newtonian viscosity fluid.
- When $We > 1$ the problems are interesting and extremally complicated.

Introduction: Stabilized formulation

Variational Multiscales Methods (VMS)

- Approximating the effect of the components of the solution of the continuous problem that cannot be resolved by the finite element mesh.
- \bullet Split the unknown as $\boldsymbol{U} = \boldsymbol{U}_h + \boldsymbol{U}'$, where $\boldsymbol{U}_h \in \mathcal{X}_h$ and $U' \in \mathcal{X}'$. The spaces \mathcal{X}_h and \mathcal{X}' are such that $\mathcal{X} = \mathcal{X}_h \bigoplus \mathcal{X}'.$

A standard problem, is exactly equivalent to:

$$
\left(M(U)\frac{\partial U}{\partial t}, V_h\right) + \langle \mathcal{L}(U, U), V_h \rangle = \langle F, V_h \rangle \ \forall V_h \in \mathcal{X}_h,
$$

$$
\left(M(U)\frac{\partial U}{\partial t}, V'\right) + \langle \mathcal{L}(U, U), V' \rangle = \langle F, V' \rangle \ \forall V' \in \mathcal{X}',
$$

Introduction: Stabilized formulation

VMS in the viscoelastic case

 $(\mathcal{D}_{t}(\boldsymbol{U}_{h}),\boldsymbol{V}_{h}) + \boldsymbol{B}(\boldsymbol{u}_{h};\boldsymbol{U}_{h},\boldsymbol{V}_{h}) + \sum_{K} \langle \tilde{\boldsymbol{U}}, \boldsymbol{\mathcal{L}}^{*}(\boldsymbol{u}_{h};\boldsymbol{V}_{h}) \rangle_{K} = \langle \boldsymbol{f}, \boldsymbol{v}_{h} \rangle,$

where

- D_t represents the temporal terms.
- \bullet B is the bilinear form of the variational problem.
- $\bullet\,\,\, \tilde{\bm U} = \alpha \tilde{P} [\textbf{F} {\mathcal{L}}(\bm u_h; \, \bm U_h)]$ where \tilde{P} is the L^2 projection onto the space of sub-grid scales, α is a matrix computed within each element and $\mathcal L$ is the operator associated to the problem.
- \mathcal{L}^* is the formal adjoint of the operator.

E. Castillo and R. Codina. Finite Element approximation of the viscoelastic flow problem: A non-residual based stabilized formulation. Computer and Fluids, 142 (2015)

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Thermal coupling: Introduction

Heat transfer processes

- Viscoelastic fluids have very advantageous properties for heat transfer and transport.
- As the Weissemberg number increases, the dynamics of viscoelastic fluid change. This turn out in a higher mixing capacity, with benefits in the heat transfer between the fluid and the pipe transporting it.
- Examples: Fire brigades water tanks, petroleum extraction, reducing the drag forces in submarines, chemical reactors.

Thermal coupling

Mathematical model

- The constitutive model used in literature for the coupling is the Phan Thien Tanner (PTT) model.
- Viscous dissipation is added in energy equation.
- Temperature dependency of the physical parameters λ and η_0 .

Energy equation
\n
$$
\rho C_p \left(\frac{\partial \theta}{\partial t} + \mathbf{u} \cdot \nabla \theta \right) = k \Delta \theta + \boldsymbol{\sigma} : \nabla^s \mathbf{u} \qquad \begin{matrix}\n\lambda(\theta) = \lambda(\theta_0) f(\theta), \\
\eta_0(\theta) = \eta_0(\theta_0) f(\theta), \\
f(\theta) = \\
\exp \left[-\frac{c_1 \cdot (\theta - \theta_0)}{c_2 + (\theta - \theta_0)} \right]\n\end{matrix}
$$

Gerrit W.M. Peters, Frank P.T. Baaijens. Modelling of non-isothermal viscoelastic flows. Journal of non-Newtonians Fluid Mechanics, 68 (1997): 205-224

Thermal coupling: Fully system of equations Momentum equation:

$$
\rho \frac{\partial \mathbf{u}}{\partial t} + \rho \mathbf{u} \cdot \nabla \mathbf{u} - \nabla \cdot \boldsymbol{\sigma} - 2 \beta \eta_0(\theta) \nabla \cdot (\nabla^s \mathbf{u}) + \nabla p = \mathbf{f} \text{ in } \Omega, t \in]0, t_f[,
$$

Continuity equation:

$$
\nabla \cdot \mathbf{u} = 0 \text{ in } \Omega, t \in]0, t_f[
$$

Constitutive equation (PTT):

$$
\frac{1}{2\eta_0(\theta)}\boldsymbol{\sigma} - (1-\beta)\nabla^s \mathbf{u} + \frac{\lambda(\theta)}{2\eta_0(\theta)} \left(\frac{\partial \boldsymbol{\sigma}}{\partial t} + \mathbf{u} \cdot \nabla \boldsymbol{\sigma} - \boldsymbol{\sigma} \cdot \nabla \mathbf{u} - (\nabla \mathbf{u}^\top) \cdot \boldsymbol{\sigma} \right) + \frac{1}{2\eta_0(\theta)} \left(\epsilon \frac{\lambda(\theta)}{(1-\beta)\eta_0(\theta)} \text{Tr}(\boldsymbol{\sigma}) \boldsymbol{\sigma} \right) = \mathbf{0} \text{ in } \Omega, t \in]0, t_f[
$$

Energy equation:

$$
\rho C_p \left(\frac{\partial \theta}{\partial t} + \mathbf{u} \cdot \nabla \theta \right) - k \Delta \theta - \boldsymbol{\sigma} : \nabla^s \mathbf{u} = 0, \text{ in } \Omega, t \in]0, t_f[
$$

Thermal coupling: Numerical Results

Algorithm employed is

- iterative
- non-monolithic
- executed in a partitioner manner.

Time descretization scheme Classical backward-difference (BDF) approximations.

$$
\delta_k g^{n+1} = \frac{1}{\gamma_k} \left(g^{n+1} - \sum_{i=0}^{k-1} \varphi_k^i g^{n-i} \right)
$$

Validation: Flow around a cylinder

Scheme of the problem.

Thermal coupling: Validation

Distribution of temperature θ (below) and stress component σ_{xx} (top) around the cylinder for We=4.

Gerrit W.M. Peters, Frank P.T. Baaijens. Modelling of non-isothermal viscoelastic flows. Journal of non-Newtonians Fluid Mechanics, 68 (1997): 205-224

Thermal coupling: Validation

Temperature θ for We=1,2 and 4 as a function of x-coordinate.

Stress component σ_{xx} , We=4, in isothermal and non-isothermal case as a function of x-coordinate.

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High Weissemberg Numbers: Turbulence

- Takes place when the elastic part of the fluid becomes relevant, that is, at high Weissemberg numbers.
- Transition to turbulence has been shown to take place earlier and at lower Reynolds number in viscoelastic solutions.
- The addition of long-chain polymers can help to reduce the turbulent friction reductions in the boundary layer.
- Examples: polymeric solutions and polymer casting.

The High Weissemberg Number Problem (HWNP)

- Computational rheology started in the early 1970s. Mostly finite-element methods for steady 2D flows.
- All methods, without exception, were found to **break down** at a "ustratingly low value" of the Weissenberg number.
- The reason for this breakdown has remained somewhat of a mystery. Evidence that it is a numerical phenomenon.
- The high-Weissenberg number problem has haunted computational rheology for over 30 years.

Logarithmic conformation reformulation (LCR)

Reformulating constitutive laws

- Was proposed by Fattal and Kupferman.
- Seeks to treat the exponential growth of the elastic stresses when the elastic component becomes dominant.
- This allows to extend the range of Weissemberg numbers.

Logarithmic conformation reformulation (LCR)

• Physically-admissible conformation tensors must, by definition, be symmetric and positive-definite.

$$
\boldsymbol{\sigma} = \frac{\eta_{\boldsymbol{p}}}{\lambda_0}(\boldsymbol{\tau} - \mathbf{I}) \longrightarrow \boldsymbol{\tau} = \frac{\lambda_0 \boldsymbol{\sigma}}{\eta_{\boldsymbol{p}}} + \mathbf{I}
$$

• The conformation tensor is replaced by a new variable $\psi = \log(\tau)$.

So, inserting the descomposition in the equation, the constitutive law transforms into

$$
\frac{1}{2\lambda_0}(\exp(\psi) - \mathbf{I}) - \nabla^s \mathbf{u} + \frac{\lambda}{2\lambda_0} (\mathbf{u} \cdot \nabla \exp(\psi))
$$

$$
\frac{\lambda}{2\lambda_0} + (-\exp(\psi) \cdot \nabla \mathbf{u} - (\nabla \mathbf{u})^T \cdot \exp(\psi) + 2\nabla^s \mathbf{u}) = \mathbf{0}
$$

Logarithmic conformation reformulation (LCR)

Consequently, the new set of equations to be solved can be written as follows

$$
-\frac{\eta_0(1-\beta)}{\lambda_0}\nabla \cdot \exp(\psi) - 2\beta \nabla \cdot (\nabla^s \mathbf{u}) + \rho \mathbf{u} \cdot \nabla \mathbf{u} + \nabla p = \mathbf{f},
$$

$$
\nabla \cdot \mathbf{u} = 0,
$$

$$
\frac{1}{2\lambda_0}(\exp(\psi) - \mathbf{I}) - \nabla^s \mathbf{u} + \frac{\lambda}{2\lambda_0}(\mathbf{u} \cdot \nabla \exp(\psi)) +
$$

$$
\frac{\lambda}{2\lambda_0}(-\exp(\psi) \cdot \nabla \mathbf{u} - (\nabla \mathbf{u})^T \cdot \exp(\psi) + 2\nabla^s \mathbf{u}) = 0
$$

Logarithmic conformation reformulation (LCR)

We have developed the linearization of LCR problem in order to design a stabilized formulation applying the Variational Multi-Scale method.

Difficulties in implementation

- Apart from the well-known non-linearities, a exponential function must be linearized.
- We have to be especially careful with convective term $\mathbf{u} \cdot \nabla$ exp (ψ) and its linearization.
- The computational cost increases because of the calculation of the exponential.

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Summarizing

- Viscoelastic fluids have a wide range of applications in industry.
- Particularly, they have a higher mixing capacity and heat transfer properties.
- Simulating viscoelastic fluid flows at high Weissemberg numbers is currently one of the biggest challenges in computational rheology.

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Women in science: statistics

Statistics from USA until 2011 in fields of STEM (Science, Technology, Engineering and Mathematics).

Women in science: statistics

Women in science: engineering and mathematics

Thank you for your attention

Laura Moreno Martínez